

Analytical results for the C-angularity soft function at NNLO

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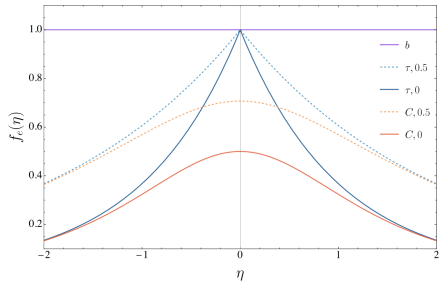
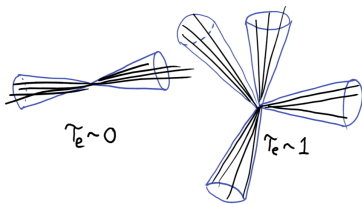
Overview

1. Motivation
2. Factorisation
3. Calculation Setup
4. Calculation

Aims

- Calculation of a soft function to NNLO in QCD
 - Piece of a cross section that describes correction due to low momentum (soft) radiation, can be combined with other pieces to get full result
 - Also gives NNLO soft anomalous dimension required for resummation
- Calculate for a new family of event shapes called "C-angularities"
 - Could be useful in extracting α_S from e^+e^- collisions
 - Includes results for C-parameter event shape
- Streamline calculation for easier N3LO calculation
 - N3LO (C-)angularity anomalous dimension last piece for N3LL resummation of (C-)angularities
 - N3LO C-parameter soft function last piece for N3LL' accuracy (Between N3LL and N4LL accuracy)

Event Shapes



- Thrust $\mathcal{T}_\tau = |p_\perp| e^{-|y|}$
 - Discontinuous derivative at $y = 0$
- C-Parameter $\mathcal{T}_C = \frac{|p_\perp|}{2\cosh(y)}$
 - Fully differentiable
- Jet broadening $\mathcal{T}_b = |p_\perp|$

- Angularities $\mathcal{T}_{\tau,a} = |p_\perp| e^{-|y|(1-a)}$
 - Varies between Thrust and Jet broadening
- C-Angularities $\mathcal{T}_{C,a} = \frac{|p_\perp|}{(2\cosh(y))^{1-a}}$
 - Varies between C-Parameter and Jet broadening

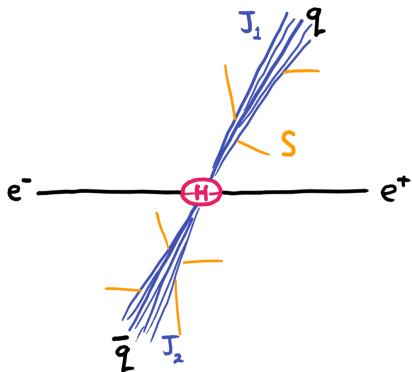
Motivation - Measuring α_S

- Event Shape distribution $\frac{d\sigma}{d\tau_e}$ can be used to determine the strong coupling constant α_S
- Fit tail of dijet region to α_S and non perturbative parameter Ω_1
 - Use different values of a to break degeneracies between α_S and Ω_1
 - Has been done with angularities [Bell et al., 2019]
 - C-angularities - simpler calculation due to smooth behaviour
- Must re-sum large logarithms that break perturbation
 - Requires anomalous dimension

SCET Factorisation

Factorisation

$$\frac{d\sigma}{d\tau_{C,a}} = H(Q, \mu) \times (S(\mathcal{T}_S, \mu) \otimes J_1(\mathcal{T}_J, \mu) \otimes J_2(\mathcal{T}_J, \mu))$$



- $S(\mathcal{T}_S, \mu)$ Soft Function
 - Soft radiation, at low energy scale \mathcal{T}_S
- $H(Q, \mu)$ Hard Function
 - Scattering process at high energy scale Q
- $J(\mathcal{T}_J, \mu)$ Jet Functions
 - Collinear final state radiation, at an intermediate energy scale \mathcal{T}_J
- $(B(\mathcal{T}_J, \mu)$ Beam functions)
 - Collinear initial state radiation + PDFs

Calculation Setup

- Integrate over soft amplitudes with measurement on real radiation
 - Has a complicated divergence structure when momenta become soft/collinear

Key Idea - Split soft function into two pieces

- "global" piece S^Σ
 - Much easier to calculate, can be extracted from kinematic limit of existing beam function results
- correction term ΔS
 - Has a much simpler divergence structure
 - can be expanded in a , coefficients can be calculated analytically

Calculation Setup - Measurement Function

Apply $\mathcal{M} = \delta(\mathcal{T}_{C,a} = \mathcal{T}_S)$ or $\theta(\mathcal{T}_{C,a} < \mathcal{T}_{\text{cut}})$ to real radiation

- Split measurement function into two pieces
- C-Angularity $\mathcal{T}_{C,a} = \sum_i \mathcal{T}_{C,a}(k_i)$
 - Correct IR safe variable
- "global" C-Angularity $\mathcal{T}_{C,a}^\Sigma = \mathcal{T}_{C,a}(\sum_i k_i)$
 - Incorrect variable (IR unsafe)...
 - ... but easier to calculate
- Splits soft function into piece using global variable plus a correction term
- $\mathcal{M}(\mathcal{T}_{\text{cut}}) = \mathcal{M}^\Sigma(\mathcal{T}_{\text{cut}}) + \Delta\mathcal{M}(\mathcal{T}_{\text{cut}})$, where
- $\Delta\mathcal{M}(\mathcal{T}_{\text{cut}}) = \theta(\mathcal{T}_{C,a} < \mathcal{T}_{\text{cut}}) - \theta(\mathcal{T}_{C,a}^\Sigma < \mathcal{T}_{\text{cut}})$

Calculation Setup - Divergences

- Momenta becoming soft/collinear produce divergences - potentially complicating calculation
- S_Σ extracted from existing NNLO beam function results, so ΔS is the only complicated bit
- For most cases, $\mathcal{T}_{C,a}^\Sigma$ and $\mathcal{T}_{C,a}$ coincide in the IR limit $\Rightarrow \Delta\mathcal{M}$ controls divergence of the amplitude

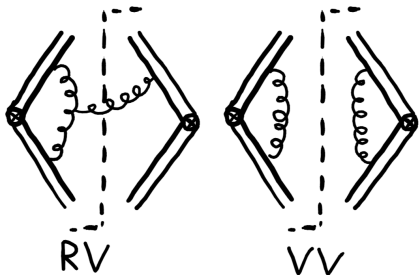
Two Exceptions!

- Each parton momentum become collinear to the opposite jet (anti-collinear)
- Total parton momenta become collinear to a jet



Calculation Setup - Amplitudes

Soft amplitudes created from two linear Wilson lines



- Amplitudes with 2 virtual loops (VV) scaleless
 $\implies S = 0$
- Amplitudes with 1 real emission, 1 virtual (RV):
 $\Delta\mathcal{M} = 0 \implies \Delta S = 0$

Calculation Setup - Amplitudes

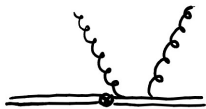


Figure 1: Uncorrelated Emission

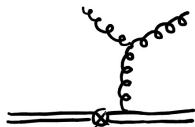


Figure 2: Correlated Emission

- Split RR diagrams into diagrams with correlated and uncorrelated emissions
- Uncorrelated emissions: emissions from different vertices, has colour factor C_R^2
 - Can be easily calculated from NLO results (non-abelian exponentiation)
- Correlated emissions: emissions from same vertex, colour factors $C_R C_A$, $C_R n_f T_F$
 - Prob. of anti-collinear emission $\rightarrow 0 \implies$ no anti-collinear divergence
 - So only one possible divergence in ΔS

Calculation Setup - Summary

- Sort amplitudes by colour factors into correlated and uncorrelated amplitudes
- $S_a^{(2,\text{uncorr.})}$ calculated from NLO result
- $S_a^{(2,\text{corr.})}$ split into $S_a^{(2,\Sigma)}$ and $\Delta S_a^{(2)}$
- $S_a^{(2,\Sigma)}$ extracted from beam function results
- Calculate $\Delta S_a^{(2)}$ for C_A and $n_f T_F$ colour factors

Calculation of $S_a^{(2,\text{uncorr.})}$ and results

- Can be calculated from convolution of NLO soft function $S^{(1)}$

$$S_a^{(2,\text{uncorr.})} = \frac{1}{2} S_a^{(1)} \otimes S_a^{(1)}$$

$$S_a^{(2,\text{uncorr.})}(\mathcal{T}_{\text{cut}}, \mu) = \frac{4C_R^2}{(1-a)^2} \left[2 \log^4 \left(\frac{\mathcal{T}_{\text{cut}}}{\mu} \right) + \frac{(-2a^2 + 4a - 11)\pi^2}{6} \log^2 \left(\frac{\mathcal{T}_{\text{cut}}}{\mu} \right) \right. \\ \left. + 16\zeta(3) \log \left(\frac{\mathcal{T}_{\text{cut}}}{\mu} \right) + \frac{\pi^4 (20a^4 - 80a^3 + 140a^2 - 120a + 13)}{1440} \right]$$

Calculation of $S_a^{(2,\Sigma)}$

- Can be calculated from existing NNLO beam function results [Baranowski, 2020]
 - Beam functions depend on the momentum fraction z
 - In the limit of $z \rightarrow 1$, the beam function produces a structure similar to the global variable soft function
 - Specifically, S^Σ can be written as

$$S^\Sigma = f(\epsilon) \int dr^+ dr^- (r^+ r^-)^{1-2\epsilon} \Theta(\mathcal{T}_{C,a}(r) < \mathcal{T}_{\text{cut}}) \quad (1)$$

where $f(\epsilon)$ is extracted from beam function results, and the integral over the total momentum $r^\pm = k_1^\pm + k_2^\pm$ is the NLO integral

$$\begin{aligned}
 S_a^\Sigma = C_R \Bigg\{ & C_A \left[-\frac{18\pi^4 (2a^2 - 4a + 1) - 201\pi^2 (4a^2 - 8a + 7)}{162(1-a)} \right. \\
 & + \frac{4(-1188a^3\zeta_3 + 3564a^2\zeta_3 - 3564a\zeta_3 + 693\zeta_3 + 1214)}{162(1-a)} \Bigg] \\
 & - \frac{4n_f T_F [15\pi^2 (4a^2 - 8a + 7) + 4(108a^3\zeta_3 - 324a^2\zeta_3 + 324a\zeta_3 - 63\zeta_3 - 82)]}{162(1-a)} \\
 & - \frac{4 \left(C_A (33\pi^2 (a^2 - 2a + 2) + 378\zeta_3 - 404) - 4 (3\pi^2 (a^2 - 2a + 2) - 28) n_f T_F \right)}{27(1-a)} \log \left(\frac{\mathcal{T}^{\text{cut}}}{\mu} \right) \\
 & \frac{8 \left((3\pi^2 - 67) C_A + 20n_f T_F \right)}{9(1-a)} \log^2 \left(\frac{\mathcal{T}^{\text{cut}}}{\mu} \right) \\
 & \left. + \frac{16(11C_A - 4n_f T_F)}{9(1-a)} \log^3 \left(\frac{\mathcal{T}^{\text{cut}}}{\mu} \right) \right\}
 \end{aligned} \tag{2}$$

Calculation of $\Delta S_a^{(2)}$

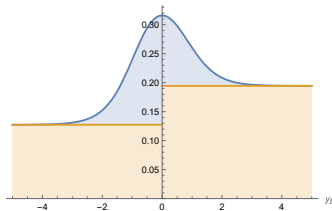


Figure 3: $C_F n_F T_F$ integrand y_t dependence. Evaluated at $\Delta y = 2$, $z = 0.5$, $a = 0.5$. Asymptotic behaviour given by orange line

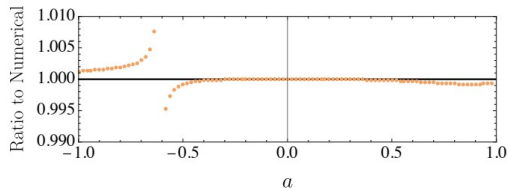
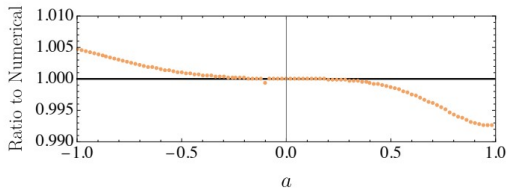
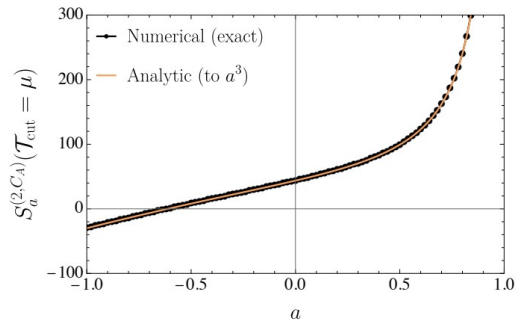
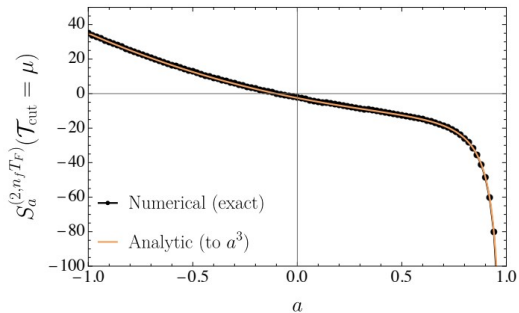
- For both C_A and $n_f T_F$ colour channels:
- Start with $8 - 2 \delta$ functions = 6 variables
- Change variables to $\cos \Delta\phi$, T , z , y_t , Δy (plus trivial ϕ_t integral)
 - The $\cos \Delta\phi$ and T integrals are simple to integrate over
 - This leaves integrals over z , Δy and y_t
- We expect a divergence as $y_t \rightarrow \pm\infty$
 - Subtract off $y_t \rightarrow \pm\infty$ asymptote (orange line), and split integrand into regularised piece I_{reg} (blue) and divergent piece I_{div} (orange)
- Finally, expand I_{div} to $\mathcal{O}(\epsilon)$ and expand both in a to desired accuracy, and perform remaining integrals

$\Delta S_a^{(2)}$ results

$I^{c,n,m}$	$c = C_R n_f T_F$	$c = C_R C_A$
$I_{\text{div.}}^{c,0,1}$	$\frac{10}{3}$	$-\frac{41}{3} + \frac{4}{3}\pi^2 + 8\zeta_3$
$I_{\text{div.}}^{c,0,2}$	$\frac{56}{45} - \frac{12}{5}\zeta_3$	$-\frac{118}{45} + \frac{1}{3}\pi^2 - \frac{24}{5}\zeta_3$
$I_{\text{div.}}^{c,0,3}$	$\frac{11}{54} - \frac{2}{9}\zeta_3$	$-\frac{65}{108} + \frac{1}{9}\pi^2 - \frac{8}{9}\zeta_3 + \frac{1}{90}\pi^4$
$I_{\text{div.}}^{c,0,4}$	$\frac{13}{210} - \frac{2}{15}\zeta_3 + \frac{1}{7}\zeta_5$	$-\frac{19}{105} + \frac{1}{24}\pi^2 - \frac{13}{30}\zeta_3 + \frac{1}{120}\pi^4 - \frac{4}{7}\zeta_5$
$I_{\text{div.}}^{c,1,1}$	$\frac{239}{9} - \frac{32}{3}\zeta_3$	$-\frac{1793}{18} + \frac{16}{3}\pi^2 + \frac{160}{3}\zeta_3 + \frac{4}{9}\pi^4$
$I_{\text{div.}}^{c,1,2}$	$\frac{2162}{225} - \frac{2}{9}\pi^2 - \frac{212}{75}\zeta_3 - \frac{1}{9}\pi^4$	$-\frac{2741}{225} + \frac{4}{9}\pi^2 + \frac{2116}{75}\zeta_3 - \frac{26}{45}\pi^4$
$I_{\text{div.}}^{c,1,3}$	$\frac{467}{1620} - \frac{1}{27}\pi^2 + \frac{202}{135}\zeta_3 - \frac{7}{405}\pi^4$	$-\frac{4187}{3240} + \frac{559}{135}\zeta_3 - \frac{31}{405}\pi^4 + \frac{2}{9}\pi^2\zeta_3 + \zeta_5$
$I_{\text{reg.}}^{c,0,0}$	$-\frac{8}{3} + \frac{16}{3}\zeta_3$	$\frac{4}{3} - \frac{44}{3}\zeta_3 + \frac{4}{15}\pi^4$
$I_{\text{reg.}}^{c,0,1}$	$\frac{25}{6} - \frac{2}{3}\pi^2 - \frac{8}{3}\zeta_3$	$-\frac{97}{12} + \frac{1}{3}\pi^2 - \frac{34}{3}\zeta_3 - \frac{11}{45}\pi^4$
$I_{\text{reg.}}^{c,0,2}$	$\frac{76}{135} - \frac{2}{9}\pi^2 + \frac{8}{225}\pi^4$	$-\frac{1021}{270} + \frac{7}{36}\pi^2 + 3\zeta_3 + \frac{13}{300}\pi^4$
$(*) I_{\text{reg.}}^{c,0,3}$	$\frac{161}{1296} - \frac{1}{27}\pi^2 - \frac{11}{54}\zeta_3 + \frac{1}{162}\pi^4$	$-\frac{5885}{2592} + \frac{5}{36}\pi^2 + \frac{127}{54}\zeta_3 - \frac{59}{3240}\pi^4 - \frac{1}{9}\pi^2\zeta_3 + \frac{1}{3}\zeta_5$

$$\Delta S_a^{(2,c)}(\mathcal{T}_{\text{cut}}, \mu) = -\frac{2I_{\text{div.}}^{c,0}}{(1-a)} \log\left(\frac{\mathcal{T}_{\text{cut}}}{\mu}\right) + \frac{I_{\text{div.}}^{c,1}}{2(1-a)} + 2I_{\text{reg.}}^{c,0} + \mathcal{O}(\epsilon)$$

Full results



Comparisons to Literature Results - Anomalous dimension

- Soft anomalous dimension γ_s - describes how a soft function changes with scale

$$\mu \frac{dS}{d\mu} = \gamma_s \otimes S$$

- Can be used to partially check $\mathcal{T}_{C,a}$ results
- Slicing variables with the same forward rapidity limit (e.g. Thrust and C-parameter) have the same anomalous dimension
- Angularities $\mathcal{T}_{\tau,a}$ coincides with $\mathcal{T}_{C,a}$ for forward rapidities, so can use the angularities anomalous dimension to check results.
- Check against [Bauer et al., 2021], all terms agree except the $C_A a^2$ - Tiny disagreement (0.2 per mille, so phenomenologically irrelevant)
 - We are in contact with the authors to hopefully solve the disagreement

Conclusion - N3LO Calculation

- Method can be used for a N3LO calculation
- Global piece can be found from limit of N3LO beam function results
- At N3LO, there are:
 - RRR, RRV, RVV and VVV diagrams
 - RVV and VVV $\rightarrow 0$ for correction piece
 - RRR can be split into CCC, CCU and UUU for correlated (C) and uncorrelated (U) emissions.
 - CCU and UUU simple to calculate like the NNLO uncorrelated piece
- Counter-terms would be necessary between RRR and RRV
- The correction piece diverges like a NLO calculation, so can modify a NLO subtraction technique

Thank you

References



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